

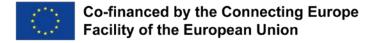






FAST DANUBE

Technical Assistance for Revising and Complementing the Feasibility Study
Regarding the Improvement of Navigation Conditions on the Romanian-Bulgarian Common Sector of the Danube and
Complementary Studies









FAST DANUBE

TECHNICAL WORKSHOP

AFDJ / IAPPD / Halcrow Romania team

29 Aug 2018, Bucuresti



Technical Workshop (29 Aug'18)

- Revised options Bechet / Corabia / Belene / Popina
- Design approach morphological principles to option selection
- Design approach river training structures / islands
- Design approach bank stabilisation
- Options appraisal modelling results
- MCA multi-criteria (objective) analysis
- Adaptive management











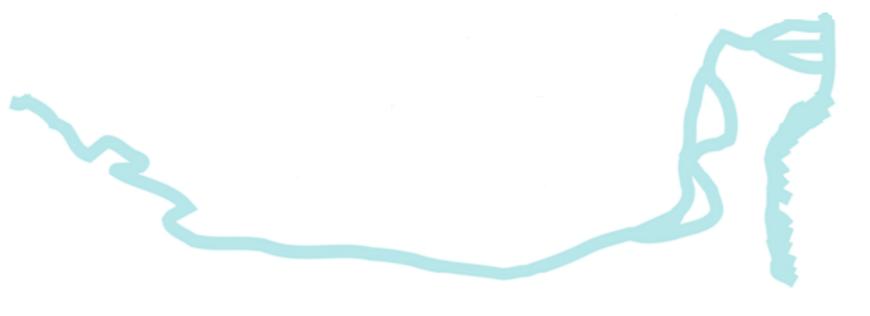
FAST DANUBE

Short presentation – TECHNICAL WORKSHOP

DESIGN APPROACH – RIVER TRAINING STRUCTURES / ISLANDS

29 Aug 2018, Bucuresti











River training structures/islands

- Feasibility designs
- Geosynthetic tubes

Best practice:

- Mississippi, US
- Lower Columbia River, US
- Kootenai/Lower Meander River, US
- Rhine, Holland (Rijkswaterstaat)
- mid-Danube, Austria (Bad Deutsch Altenberg/Witzeldorf Project between Vienna and Bratislava – deregulation of the river ie environmental restoration involving Prof Habersack)

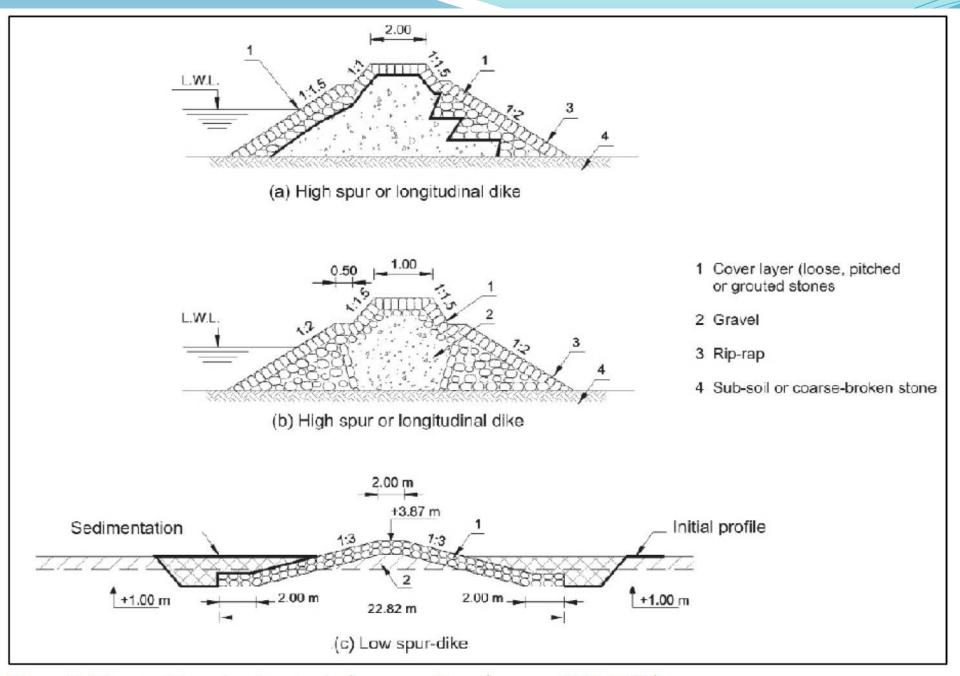
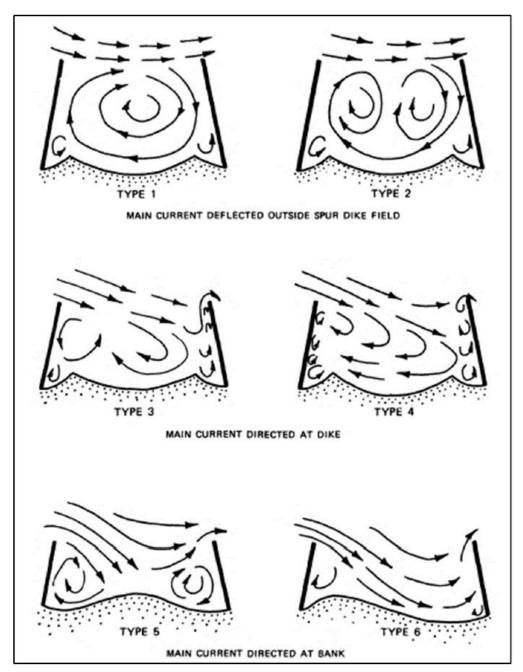


Figure 8: River training structure typical cross sections (source: CIRIA C683)





Pilot project Witzelsdorf – all construction from river

Figure 6: Flow patterns between dikes (source: Bank protection techniques using spur dikes)



Island building, Wachau, River Danube (source: Life Nature Wachau, 2008)



Island building, Bonners Ferry Island project (source: Lower Meander Project Design Report, RDG 2017)



Cutter suction dredging



Causeway construction



Core material

Options for sourcing the main core of a new island are:

- <u>Dredged from the river channel</u>: Sand and gravel dredged from the adjacent river bed using a cutter suction dredger and pumped directly onto existing sand bars. Some sand maybe swept downstream by the current during placement construction should take place during low flow periods. Large earth moving equipment will be used to shape the island as required.
 - This option requires a large quantity of material to be removed from the river bed and this could include a significant overdig of the fairway to ensure long term navigation improvements. Cutter suction dredging would not be suitable if the river bed is formed from cohesive material or rock. If necessary a sand filled bag/tube or rock containment bund could be placed around the perimeter of the island to provide tranquil conditions inside for depositing dredged material
- <u>Borrow pit</u>: Rock or earth will be excavated from a nearby landside borrow pit, transported to the river then along a causeway to the proposed island location and tipped in place. Large earth moving equipment will be used to shape the island as required

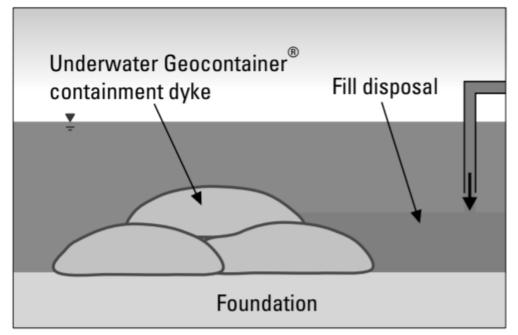




Geosynthetic tubes (geo-tubes)

Example of construction option using sand filled geosynthetic tubes for initial building of islands, dikes, groynes and chevrons:

https://www.rhmooreassociates.com/images/pdf/Geotube-BRO_CoastalAndMarine_tcm28-43898.pdf



•Geobag system; 2 till 10 m³

•Geotube® system; 100 tot 750 m³

•Geocontainer® system; 100 tot 600 m³

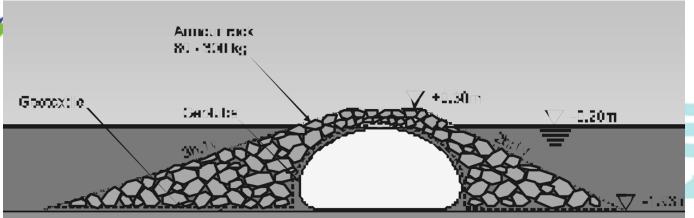
Geosystems are sand filled elements made out of woven high strength textiles. The textiles used are special designed for Geosystems with the same strength in both directions.

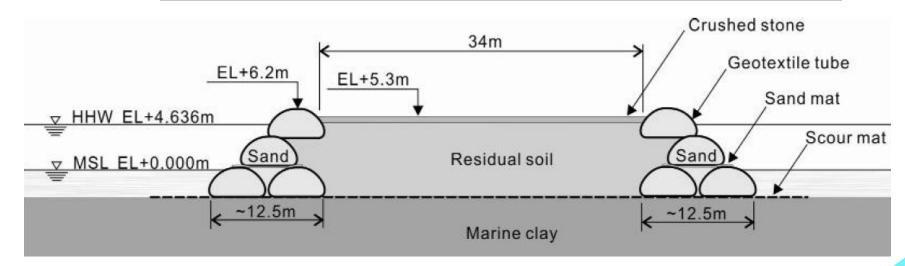
In some instances, underwater containment dykes are constructed to retain spoil and other fills in an environmentally acceptable manner.

Underwater Geocontainer® containment dyke





















Geotube[®] system

- Will be filled on position.
- Filling hydraulically with a mixture of sand and water.
- Lengths vary between 30 till 100 meter.
- Diameter vary between 1,6 till 5 meter diameter.
- In relative short period a dam can be constructed.
- Essential is fabric strength and confection, seam strength.

diameter	circum	height	fill	width	width	recommended
				max	base	high strength
D	С	Н	F	W	Wb	fabric
m	m	m	m3/m1	m	m	
1,60	5,0	1,0	1,7	2,0	1,7	GT 750 M
2,50	7,9	1,5	4,1	3,2	2,7	GT 750 M
3,25	10,2	2,0	6,9	4,2	3,5	GT 1000 M
4,00	12,6	2,4	10,4	5,1	4,3	GT 1000 M
5,00	15,7	2,7	16,3	6,4	6,0	GT 1000 M
			•			







Dawlish Warren Beach Management Scheme

Project update

September 2017



16

















































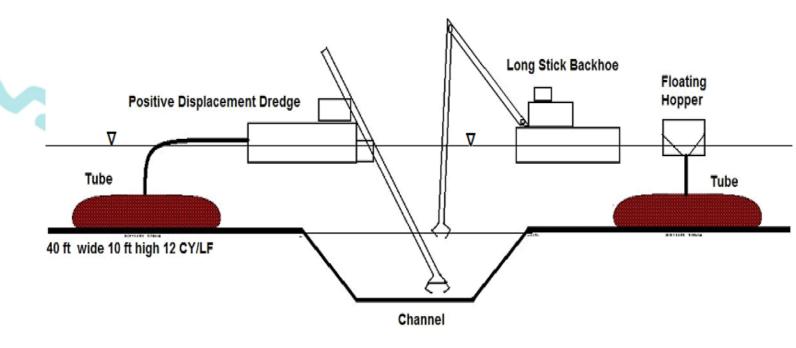








Filling Tubes Underwater









Installation/filling time

Giving: Geotube® diameter 4 meter fillingheigth 2,4 meter, length 50 meters.

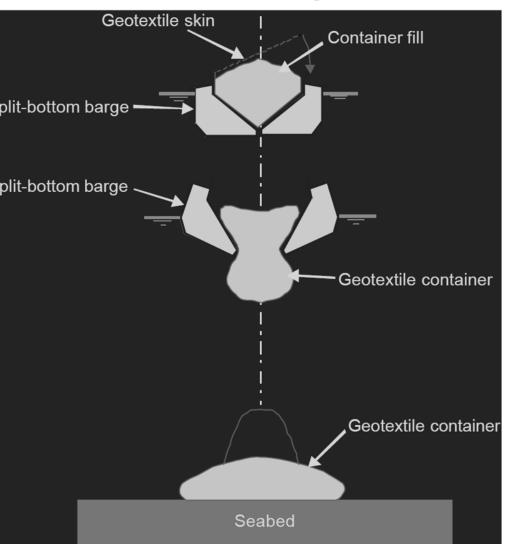
Total volume to be filled with $50 \times 10,4 = 520 \text{ m}$ 3

pumpcapacity 400 m3/hour at 15 % mixture (60 m3/hour)

It will take around 520/60= 9 hours to fill the Geotube®.

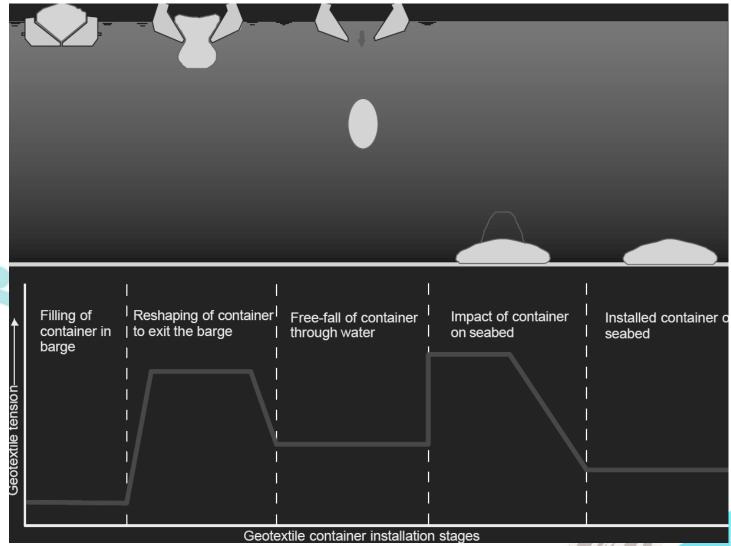


Geocontainer® system

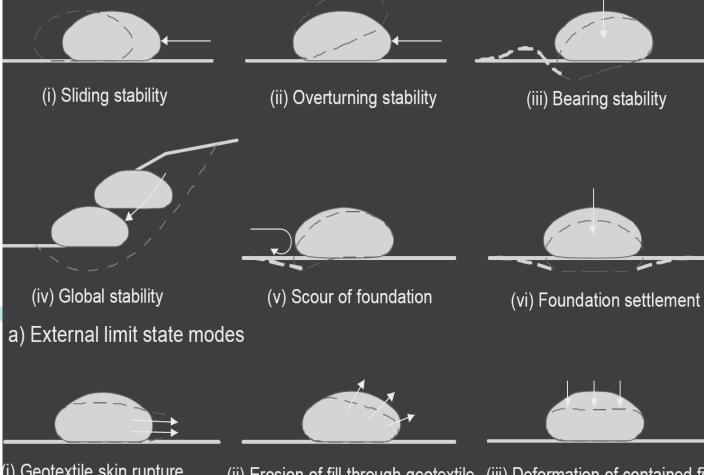


- Geocontainer® are installed by split-bottom barges
- Two types of applications:
 - Structural, submarine, mass-gravity units
 - Contained, submarine disposal of contaminated sediments
- For hydraulic applications container volumes are in range 100 to 600 m³
 - Smaller volumes give better installed tolerances and are more easily installed but are more costly









- (i) Geotextile skin rupture
- (ii) Erosion of fill through geotextile (iii) Deformation of contained fill skin
- b) Internal limit state modes





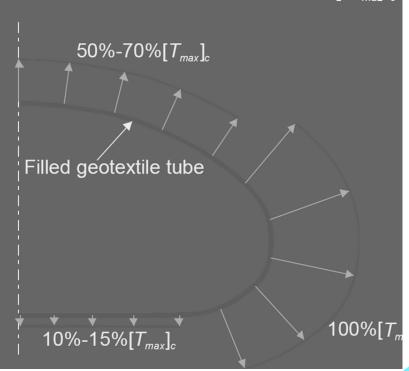
a) Circumferential tension distribution around a filled geotextile tube

Circumferential tension distribution around filled geotextile tube

Filled géotextile tube

Location of maximum circumferential tension

b) Approximation of circumferential tension distribution in terms of $[T_{ma}]_c$









- Circumference of tube, L=9 m
- No outside water
- $\gamma_{\text{slurry}} / \gamma_{\text{water}} = 1.2$
- No safety factors on geosynthetic strength

